

Fig. 25—Diagrams illustrating the orientation of the axes of compression ( $\sigma'_1$ ) and extension ( $\sigma'_3$ ) that would be most effective in causing twin gliding on  $e\{0112\}$  in calcite. (a) The plane of the diagram is perpendicular to the gliding plane and contains the gliding direction, the  $c_v$ , and the normal to the gliding plane ( $e$ ). (b) Lower hemisphere, equal-area projection of the relationships in (a) are shown for two differently oriented cases.

therefore, the positions of  $\sigma'_1$  and  $\sigma'_3$  for  $S_o = 0.5$  can be determined (Fig. 25(b)) by measuring and plotting  $e_1$  and  $c_v$ .

Twinning can, of course, be initiated for  $S_o$  values less than 0.5 as long as  $\tau_c$  is exceeded and the correct sense is maintained. For example, the average  $S_o$  value is 0.27 for the twinned calcite cement of an experimentally deformed sandstone.<sup>(59)</sup> Turner's technique utilizes  $S_o = 0.5$ , however, because this value allows unique location of the principal stresses. (There are an infinite number of possible orientations for the stress axes for  $S_o < 0.5$ .) Moreover, there is a good empirical relationship between the amount of twinning and  $S_o$  values. In experimentally deformed Yule marble and Hasmark dolomite, the greatest amount of twinning occurs on that set of twin gliding planes for which the resolved shear-stress coefficient was highest (Fig. 26).<sup>(52,106)</sup>

The technique using calcite twin lamellae to derive the orientations of the principal stresses in a rock consists of the following steps. (1) The orientation of the best developed set of twin lamellae and the host  $c_v$  in each grain are determined by universal-stage

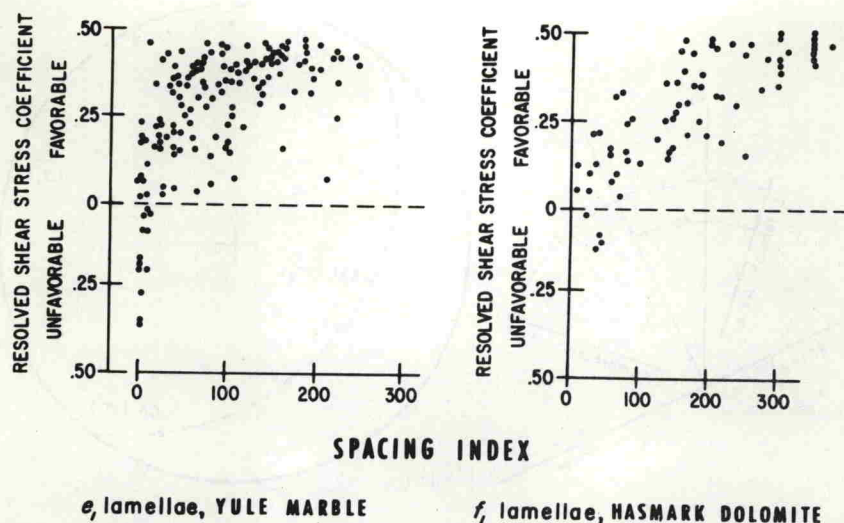


Fig. 26—Plots illustrating the relationship between  $e_1$  and  $f_1$  twin-lamellae spacing indices and  $S_0$  values for these planes as calculated from the known stress orientations in experimentally deformed Yule marble and Hasmark dolomite, respectively (from Turner and Ch'ih, Ref. 106, Fig. 6; and Handin and Fairbairn, Ref. 52, Fig. 6, respectively). Twin-lamellae spacing index is defined as the number of lamellae per millimeter when viewed on edge.

measurements. (2) These data are plotted in equal-area projection, and the compression and extension axes are located for each grain as outlined above. (3) The data measured in two or more mutually perpendicular thin sections are combined into a composite diagram, and the resulting orientation pattern is interpreted as reflecting the average orientation of  $\sigma_1$  and  $\sigma_3$  in the rock at the time twinning took place. Friedman<sup>(59)</sup> has found good agreement between the derived position of  $\sigma_1$  and the known orientation of  $\sigma_1$  in experimentally deformed calcite-cemented sandstones (Fig. 27).

A readily visible example of this technique is described by Friedman and Conger.<sup>(112)</sup> Calcite crystals within the walls of a naturally deformed fossil shell (Fig. 28) exhibit in thin section a systematic development of  $e$  twin lamellae. In transverse section the walls are elliptical and the crystals along two opposite sides of the ellipse (each encompassing 120 degrees of arc) are profusely twinned, whereas those along the two remaining 60-degree arcs are sparsely twinned. Calcite  $c_v$  are oriented radially. Fig. 29(a) shows that the preferential development of twin lamellae probably depends on favorable